

Exploring in situ U-Value thermal performance of glazing with infrared thermography for an urban multifamily housing complex

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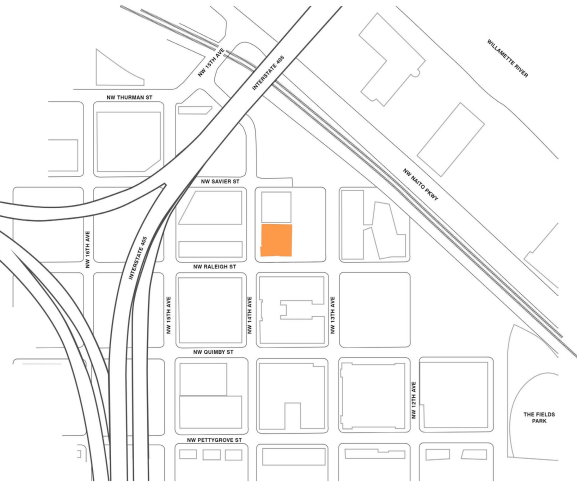
ARCH 563
WINTER 2020

Research Questions |

- 1. How is the exterior glazing performing compared to the anticipated U-values.*
- 2. Are there any portions of the building envelope that are "thermal holes".*
- 3. How does the envelope impact the building's energy use?*
- 4. Are there design strategies to make the envelope more efficient?*

Vibrant! | Portland, OR

Salazar Architects Inc.



SITE PLAN

0 100' 200' 400'



1) INTERNATIONAL & NATIONAL
STANDARDS
(ISO, ASHRAE, ANSI, NFRC)

2) REGIONAL CODE REQUIREMENTS
(TITLE 24, OEESC - 2014-19)

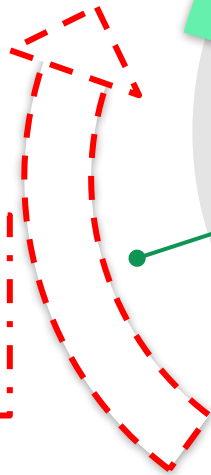
**Incomplete U-Value
Feedback Loop**

3) MANUFACTURER SPECIFICATION
(Designed to International and
National Standards)

4) ARCHITECTS / CONSTRUCTION

(Designed to Regional and State Code
Requirements)

5) POST-OCCUPANCY EVALUATIONS
(Attempted measuring of actual
building performance)



U-Value Calculations

Theoretical

In-Situ

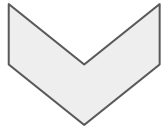
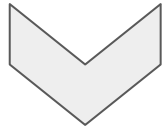
ISO 6946

ISO 15099

ISO 10077

ISO 9869

Experimental



Just Calculation

Just Calculation

Just Calculation

Calculation + Measured

Calculation + Measured

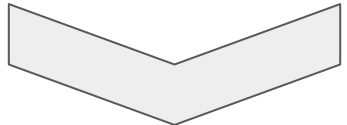
Wall Stratigraphy

NFRC Window

Passive House Window

Heat Flux Meter Wall Stratigraphy

Infrared Thermography Window



Equation #1

Equation #2


Equation #3

Equation #4

**Equation used in the current research*


Equation #1 ISO 6946 | Calculation for Building Stratigraphy

ISO 6946



Just Calculation

Wall Stratigraphy



Equation #1

$$U = \frac{1}{R_T} = \frac{1}{R_{se} + \frac{d_1}{\lambda_1} + \frac{d_2}{\lambda_2} + \dots + R_{si}}$$

U: heat transfer coefficient

R_T : total thermal resistance

R_{SE} : external resistance

d_i : thickness of the layer

λ_i : specific thermal conductivity of this layer

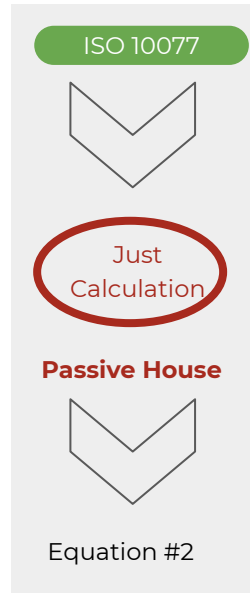
R_{si} : internal heat transfer resistance

$$R_s = 1/H_c + H_r$$

H_c = is the convective coefficient

H_r = is the radiative coefficient

Equation #2 ISO 10077 | Calculation for Glazing or Windows



$$U_w = \frac{A_g U_g + A_f U_f + l_g \Psi_g (+ l_{inst} \Psi_{inst})}{A_g + A_f}$$

U_w : heat transfer coefficient (window unit)

A_g : glazing surface area

U_g : U-value of glazing

A_f : surface area of frame

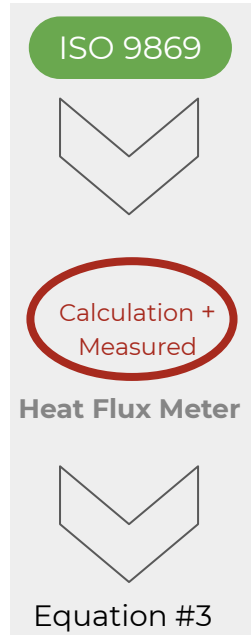
U_f : U-value of frame

l_g : glazing perimeter (glass edge length)

Ψ_g : thermal bridging coefficient of glazing

l_{inst} : frame perimeter (frame edge length)

Ψ_{inst} : thermal bridging coefficient of installation



Equation #3 ISO 9869 | In-Situ Calculation using Heat Flux Meter

$$U\text{-Value} = h_{ci} \frac{T_i - T_{si}}{T_i - T_e}$$

U: heat transfer coefficient

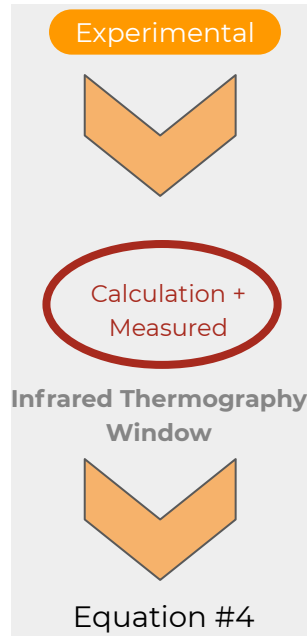
h_{ci} : surface convective heat transfer coefficient

T_i : indoor ambient temperature

T_{si} : interior surface temperature

T_e : outside ambient temperature

Experimental | In-Situ Calculation using Infrared Thermography



**Equation used in the current research*

$$U = \frac{5.67 \epsilon_{tot} \left[\left(\frac{T_w}{100} \right)^4 - \left(\frac{T_{out}}{100} \right)^4 \right] + 3.8054 v (T_w - T_{out})}{(T_{int} - T_{out})}$$

U: heat transfer coefficient

ϵ_{tot} : emissivity of specific material

T_w : surface temperature

T_{out} : ambient outside temperature

T_{in} : ambient inside temperature

V: velocity of wind

5.67: Stefan Boltzmann constant for radiative heat transfer coefficient

3.8054: convective heat transfer coefficient

Typical In Situ Deviation From Theoretical Calculations Using Infrared Thermography compared to other methods

40-45%

IRT (infrared thermography)

This numbers are typically from building stratigraphy case studies. Not specified as glazing case studies. This is the deviation from using ISO calculations.

- No standardized equation
- Measurement recording errors
- Includes emissivity of surfaces
- Faster testing times
- Can see visual components being tested

30-35%

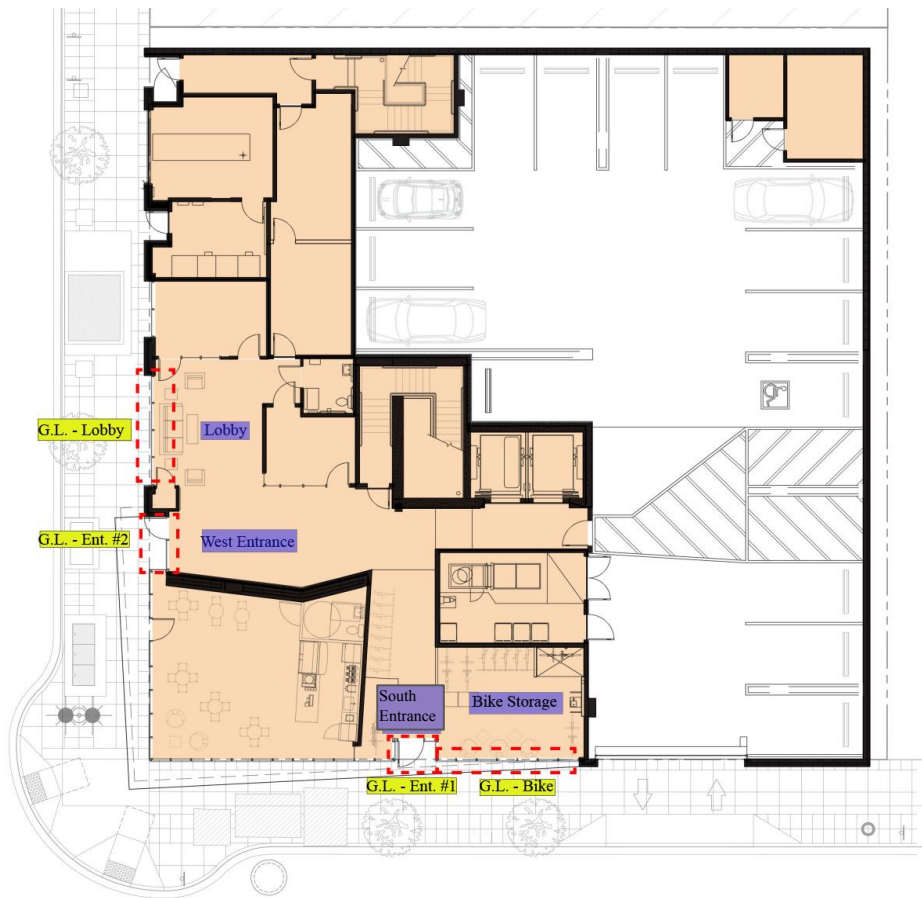
Heat Flux Meter

This number is the deviation from using ISO standardized calculations.

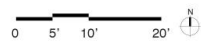
- Only measures one location at a time
- Does not include emissivity of surfaces
- Expensive equipment
- Study over long periods of time

Takeaway |

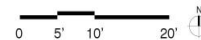
- *There is a documented difference, indicated by previous research, from theoretical calculations to in situ calculations for U-values.*
- *U-Value deviations are found even when using different in situ equipment and ISO standardized calculations. HFM shows deviations of 30-35% from theoretical calculations*



FIRST FLOOR PLAN



SECOND FLOOR PLAN



Infrared Thermography Data Collection | Representative Example



G.L. - Bike Window Type- Curtain Wall
FLIR Thermal Image: Data Collection Day #1



G.L. - Bike Window Type - Curtain Wall
FLIR Picture: Data Collection Day #1

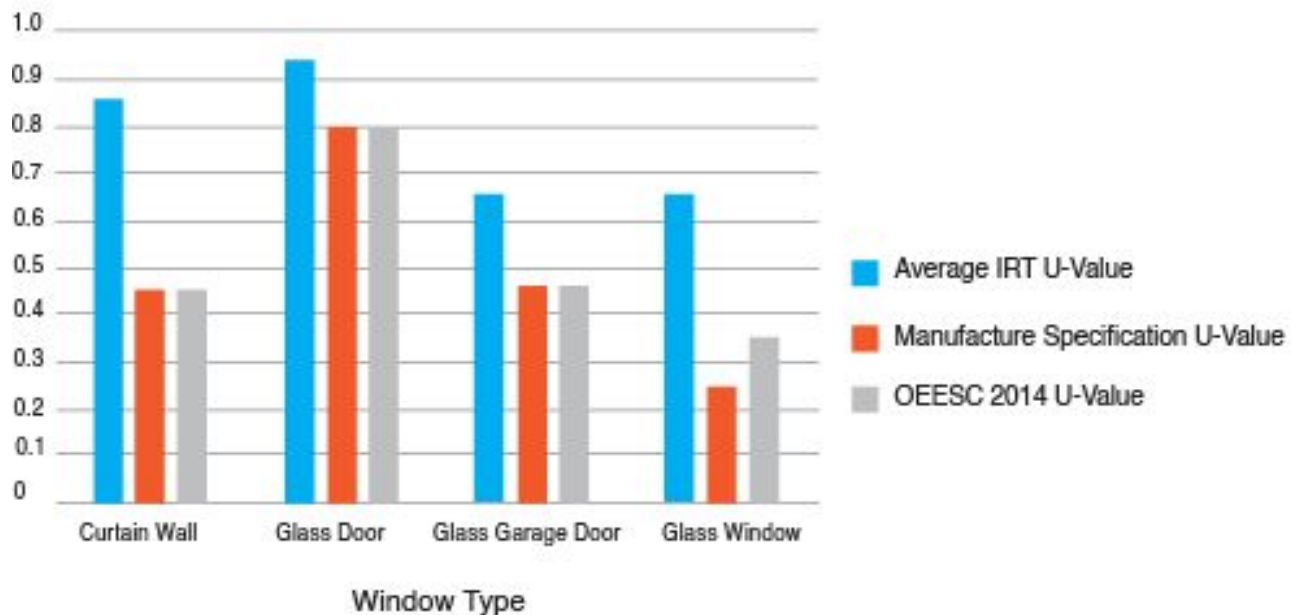
Data Collection Information					
Date:	Time:	Outside Temperature:	Inside Temperature:	Wind Velocity:	Weather Condition:
2.13.2020	10:30am - 11:30am	43°F	73°F	3.0 m/s	Cloudy
2.21.2020	10:30am - 11:30am	46°F	73°F	1.0 m/s	Sunny

U-Value Calculations using temperature recording from IRT [Table 3]

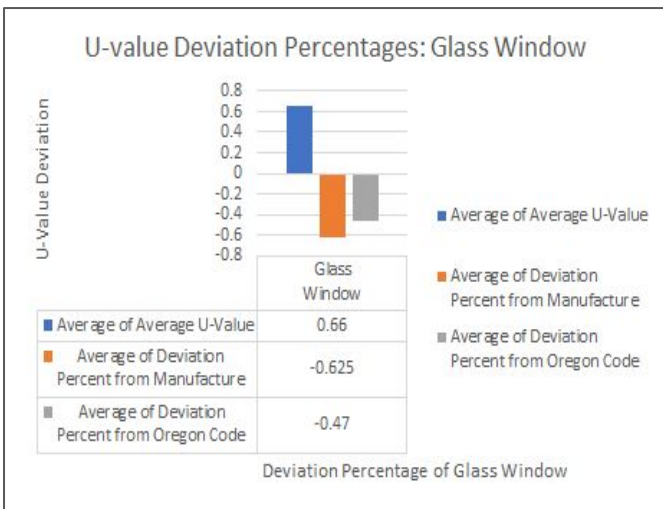
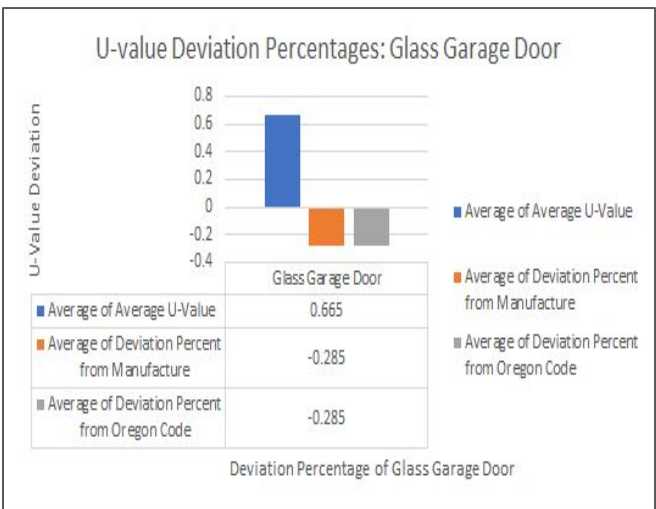
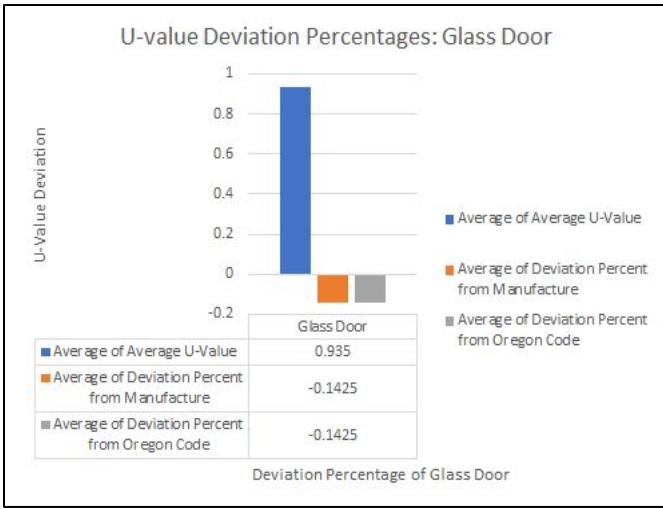
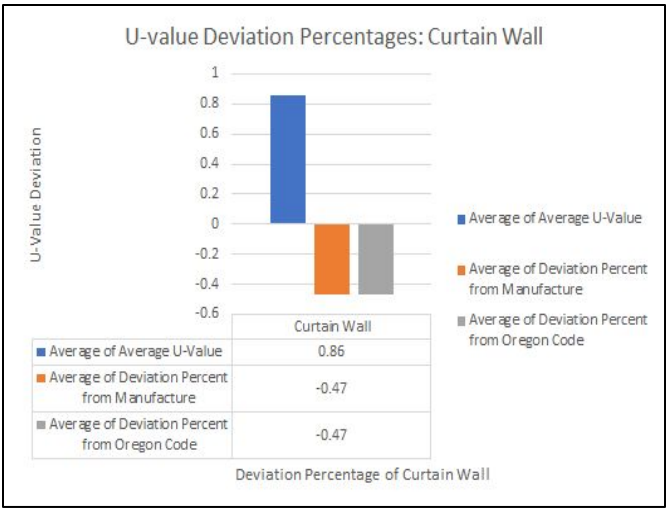
<i>Location I.D.</i>	<i>Glazing Classification:</i>	<i>Recorded (F) Day 1</i>	<i>U-Value Day 1</i>	<i>Recorded (F) Day 2</i>	<i>U-Value Day 2</i>	<i>Δ Day 1 & 2 U-Values</i>
G.L. - Bike	Curtain Wall	59	.82	61	.86	5%
G.L. - Ent. #1	Glass Door	60	.87	62	.92	5%
G.L. - Ent. #2	Glass Door	61	.93	63	.98	5%
G.L. - Lobby	Curtain Wall	62	.98	63	.98	0%
L.2 - Bike #1	Glass Door	*n/a	*n/a	*n/a	*n/a	*n/a
L.2 - Bike #2	Glass Window	57	.71	57	.63	11%
L.2 - Bike #3	Glass Window	55	.61	58	.68	10%
L.2 - Kids #1	Glass Door	62	.98	63	.98	0%
L.2 - Kids #2	Glass Garage Door	59	.82	59	.74	10%
L.2 - Comm. #1	Glass Door	61	.93	61	.86	8%
L.2. - Comm. #2	Curtain Wall	57	.72	60	.80	10%
L.2 - Comm. #3	Glass Garage Door	52	.47	55	.51	25%
L.U.308 - Main	Glass Window	59	.82	*n/a	*n/a	*n/a
L.U.308 - Bedroom	Glass Window	58	.77	*n/a	*n/a	*n/a
L.U.502 - Main	Glass Window	61	.93	*n/a	*n/a	*n/a
L.U.502 - Bedroom	Glass Window	60	.87	*n/a	*n/a	*n/a

Ground Level
 Level 2
 Living Units
 * Data was not collected

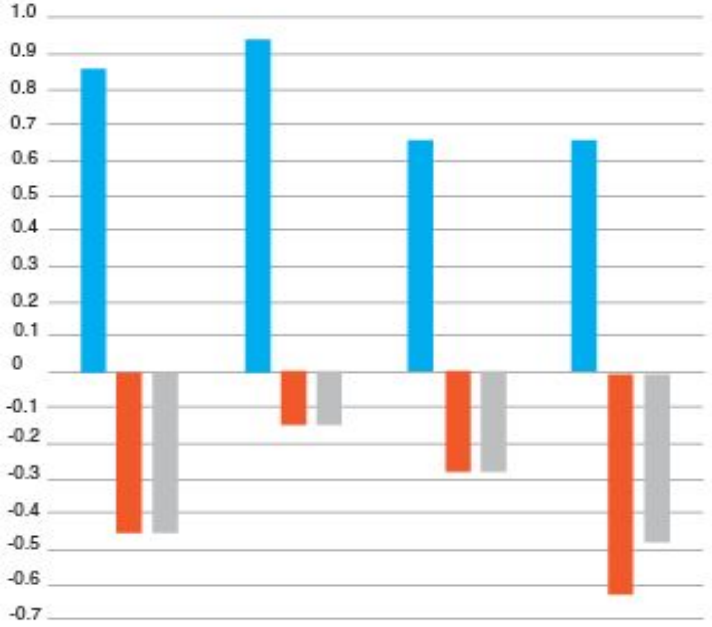
U-Value Comparison | IRT, Manufacture and OEESC



*Takeaway |
 Deviations in U-values
 from IRT to Manufacture
 and OEESC-2014 per
 individual window type*



U-Value Average Deviation | IRT, Manufacture and OEESC



- Average IRT U-Value
- Average Deviation from Manufacture Specification
- Average Deviation from OEESC 2014

	Curtain Wall	Glass Door	Glass Garage Door	Glass Window
■ Average U-Value	0.86	0.935	0.665	0.66
■ Deviation Percent from Manufacture	-0.47	-0.1425	-0.285	-0.625
■ Deviation Percent from OEESC 2014	-0.47	-0.1425	-0.285	-0.47

Takeaway:

- Curtain Wall | 47%
- Glass Door | 14%
- Garage Door | 29%
- Glass Window | 47% - 63%

IRT Expected Deviation
40% - 45%

Infrared Thermography Data Collection | Representative Example

Data Collection: Day #1

U-Value Calculations	
IRT	.82
Manufacture	.45
OEESC	.45



G.L. -Bike Window Type - Curtain Wall
 FLIR Thermal Image: Data Collection Day #1 (above)
 Data Collection Day #2 (below)



G.L. - Bike Window Type - Curtain Wall
 FLIR Picture: Data Collection Day #1 (above)
 Data Collection Day #2 (below)

Data Collection: Day #2

U-Value Calculations	
IRT	.86
Manufacture	.45
OEESC	.45



Data Collection Limitations

- Wall should be greater than the outdoor environment temperature (< 2 F)
- The difference between the indoor environment temperature and outdoor environment temperature should be at least (10-15)
- Limit direct solar irradiation
- Weather must be “fair” (clear sky, possibly sunny and non-rainy or windy)
- Wind speed must be lower than 1 m/s
- Typical climate of the site. Humidity values can significantly alter the thermal performance of the building material.
- Proper installation of the building elements in construction
- Managing of the building by users (heating/cooling and windows opening/closing)
- Maintenance work
- Measurements should be done only during evening; best time is 3:00am - 4:00am

Future Research with IRT for U-Values

- Data collection over times of year (winter and summer) show differences in U-values results using IRT.
- IRT data was collected anywhere from 3 -10 days with averages calculated for surface temperatures
- Researchers have indicated using both HFM and IRT for in-situ U-value calculation. (Power in different equipment strategies and calculations)
- Equations for U-value based on IRT is still in development. 2019 most recent research article.
- More studies need to specifically include glazing parameters in IRT calculations, most are for building stratigraphy.

Takeaway |

IRT over the last 30 years has mostly been used for qualitative data collection, however over the last 10 years it has been used for quantitative in situ measurements. These experimental calculations are still not yet applicable to average users and are not yet standardized by the industry.

However, a difference between design U-values and in situ U-values are evident from previous research

Takeaway |

- 40% of energy consumption comes from residential and commercial buildings
- U-value are one of the most important calculations for determining the performance of the buildings envelope.
- Cost of the evaluation was cited as the largest barrier to use, followed by logistical or time constraints. While portions of the market may support costs of \$5,000 or above, some key markets may require much lower costs, e.g. \$2,000.
- Areas of improvement are in creating more incentive programs for POE research to give owners more options. Additionally firms could incorporate POE research into their service package.
- Organizations like Passive House are moving away from established systems and creating their own metrics and operations for energy performance. (Needs to be scaled up and more approachable)

